

# Preparation of activated red mud and its application for removal of hydrogen sulfide in air

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## ABSTRACT

Red mud is a highly alkaline solid waste from the Bayer process for aluminum production. Red mud reservoirs are usually considered as a potential environmental risk. The treatment of red mud is costly due to the lack of an effective and economical treatment technology. On the other hand, the main components of red mud are  $\text{Fe}_2\text{O}_3$ ,  $\text{Al}_2\text{O}_3$ ,  $\text{SiO}_2$ , and  $\text{Na}_2\text{O}$ , which could be employed as a promising precursor for the preparation of various nanomaterials. In this study, we prepared activated red mud by thermal and acid treatment method and applied it for adsorption of  $\text{H}_2\text{S}$  in air. The red mud was activated under different temperatures (i.e., 200, 400, 600, and 800 °C for 4 h), types of acid (i.e.,  $\text{H}_2\text{SO}_4$  and  $\text{HCl}$ ), and acid concentrations (i.e., 0.5, 1.5, and 2.5 M). The produced materials were then applied for  $\text{H}_2\text{S}$  removal in air with concentration of 90 – 110  $\text{mg}/\text{m}^3$  using a fix-bed adsorption column test. Results showed that red mud activated at 800 °C and with 1.5 M  $\text{H}_2\text{SO}_4$  solution had the highest adsorption capacity of 29.38  $\text{mg}/\text{g}$  with an average removal efficiency of 80.2%. The effects of gas flow rate and initial  $\text{H}_2\text{S}$  concentration were also investigated, and the highest removal capacity was achieved at an inlet concentration of 100  $\text{mg}/\text{m}^3$  and flow rate of 1 L/min. Both Langmuir and Freundlich adsorption isotherms were employed for modelling the  $\text{H}_2\text{S}$  adsorption by this material and the experimental result was more fitted with the Langmuir isotherm. The thermal desorption and recyclability test were also conducted for evaluating the practical application of activated red mud material and 200 °C was the suggested desorption temperature with 81.7% adsorption capacity recovery.

**Key words:** red mud, hydrogen sulfide, adsorption, air pollution control

## INTRODUCTION

Hydrogen sulfide ( $\text{H}_2\text{S}$ ) is a toxic and colorless gas with a very unpleasant odor that originated from both nature and human activities. It greatly affects the air quality and also causes the corrosion of equipment and pipes<sup>1</sup>.  $\text{H}_2\text{S}$  is a common pollution gas in industry, biogas, coal storage, and in the processes that release odor such as sewage systems, wastewater treatment, and solid waste composting<sup>2</sup>. Air pollution due to  $\text{H}_2\text{S}$  gas is a problem that has been mentioned in lots of documents and research works<sup>3</sup>. For  $\text{H}_2\text{S}$  treatment, many methods were studied and applied such as absorption, oxidation, and biofiltration<sup>4</sup>. Among them, adsorption is considered as a simple but effective method. Therefore, finding a new, effective, and inexpensive adsorbent for  $\text{H}_2\text{S}$  removal is of interest.

On the other hand, red mud is a highly alkaline solid waste with pH from 10 – 12 from the Bayer process for aluminum production<sup>5,6</sup>, which requires a large amount of  $\text{NaOH}$ <sup>7</sup>. It comprises very fine-grained

particles with a size of < 10  $\mu\text{m}$  and a specific surface area of about 10 - 30  $\text{m}^2/\text{g}$ <sup>8</sup>. The main components of red mud are  $\text{Fe}_2\text{O}_3$ ,  $\text{Al}_2\text{O}_3$ ,  $\text{SiO}_2$ , and  $\text{Na}_2\text{O}$ . Many studies showed that red mud has a good adsorption capacity, particularly when activated by acid, heat, or combining activation with other metal oxides<sup>9-13</sup>. Currently, the research of using red mud to adsorb  $\text{H}_2\text{S}$  emission is still limited<sup>14</sup>. Therefore, in this study, we aimed to collect red mud from Tan Rai bauxite plant and then activate it by acid and thermal treatment for  $\text{H}_2\text{S}$  adsorption. Besides, other factors were also investigated such as flow rate and input concentration as well as the absorption and reuse of the adsorbent.

## MATERIALS AND METHODS

According to the study of Minh<sup>15</sup>, the pH of raw red mud from Tan Rai bauxite plant was very high at pH 11.5. Their X-ray diffraction analysis showed that the phase composition of raw red mud is mainly gibbsite (Gi)  $\gamma\text{-Al}(\text{OH})_3$ , goethite (Go)  $\alpha\text{-FeOOH}$ , and hematite (He)  $\alpha\text{-Fe}_2\text{O}_3$ <sup>15</sup>. The elemental composition of red mud includes Fe, Al, O, Na, C, Si, Ca, Ti,

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and S with a weight percentage of 18.00, 6.85, 55.21, 7.62, 8.37, 2.42, 0.21, 1.00, and 0.32 %, respectively. The collected dry red mud was firstly ground and sieved to the size of 0.097 - 0.450 mm. The material was then calcined at different temperatures of 200, 400, 600, and 800 °C for 4 h. Calcined red mud was subsequently activated with H<sub>2</sub>SO<sub>4</sub> or HCl solutions at different concentrations of 0.5, 1.5, and 2.5 M according to a process published in the literature<sup>16,17</sup>. The produced materials were denoted as RMXC-Y (activated by HCl) and RMXS-Y (activated by H<sub>2</sub>SO<sub>4</sub>) where X represents the calcined temperature (e.g., X = 4 for 400 °C) and Y is the concentration of acid. In this study, commercial activated carbon (AC) with a size of 0.097 - 0.45 mm was also prepared and employed as reference material.

The schematic for the H<sub>2</sub>S adsorption test is illustrated in Figure 1. H<sub>2</sub>S gas is generated by slowly adding of H<sub>2</sub>SO<sub>4</sub> solution to a reactor containing Na<sub>2</sub>S solution. The generated gas with a flow rate of 0.05 - 0.20 L/min was then mixed with clean air to reach the desire H<sub>2</sub>S concentration before passing through the adsorption column with an internal diameter of 16 mm made of acrylic material. A glass wool ball was employed to support an adsorbent layer of 15 - 25 mm height. The superficial airflow velocity in the column was calculated to be about 0.2 m/s and the flow was controlled in the range of 1.0 - 3.0 L/min depending on the experiments. H<sub>2</sub>S gas in the inlet and outlet was sampled and analyzed according to TCN 676 – 2006 (hydrogen sulfide determination process in the air at cattle farm of Ministry of Agriculture and Rural Development, Viet Nam), which are referenced from Methods of air sampling and analysis<sup>18</sup>. The sampling device included two impingers connected sequentially to sample H<sub>2</sub>S gas for analysis and concentration determination. Most of the experiments were conducted three times, and the average values and errors are presented in the results.

## RESULTS AND DISCUSSION

### Adsorption test

The adsorption tests were conducted with 29 different materials, including activated carbon, thermal activated red mud, and acid activated red mud. The H<sub>2</sub>S concentration was in range of 90 – 110 mg/m<sup>3</sup> and 3 g of adsorbent was used. The results are presented in Figure 2.

As seen in Figure 2, the adsorption capacity of most adsorbents derived from red mud was higher than that of AC except for RM2, RM2C-0.5, and RM4 materials. It is also obvious that the adsorption capacity of the thermally treated materials is proportional

to their activation temperature. Under high temperature, there was a phase transformation of red mud component (e.g., goethite to hematite) and the join of aluminum into the material lattice to form Al-hematite<sup>15</sup>, which acts as internal adsorption sites. In addition, since water is removed from the material at the high temperatures, the pore system is enhanced, and the material surface area could be improved.

For acid-activated red mud, it is reported that the specific surface area of material increases while the particle size tends to decrease with the acid concentration<sup>15</sup>. Therefore, the adsorption capacity also increases with the increases of acid concentration in a certain range but then decreases due to the material structure disruption under high acidic treatment condition. Besides, H<sub>2</sub>SO<sub>4</sub> was proved to be more effective than HCl for activating of red mud in terms of H<sub>2</sub>S adsorption, possibly due to the higher volatility of HCl than H<sub>2</sub>SO<sub>4</sub>. Among all materials, RM8S-1.5 had the highest H<sub>2</sub>S adsorption capacity of 29.38 mg/g, which was about 1.4 times better than that reported by Sahu *et al.*<sup>14</sup>.

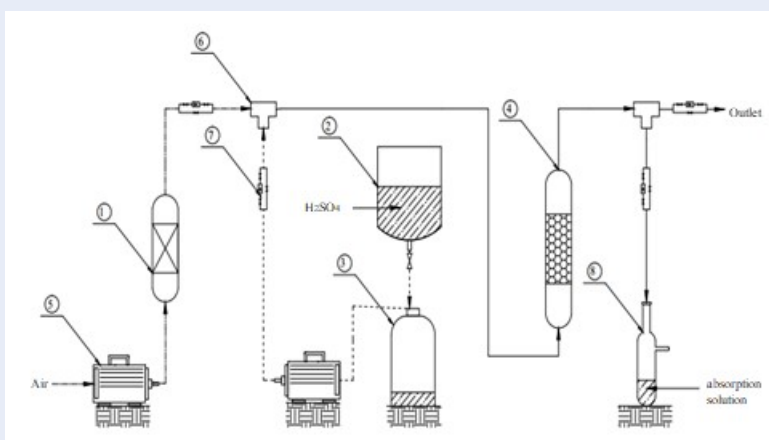
### Isotherm study

RM8S-1.5 material was then chosen for isotherm study with input H<sub>2</sub>S concentration from 40 to 120 mg/m<sup>3</sup>. As seen in Figure 3, the adsorption capacity increases when input H<sub>2</sub>S concentration increases from 40 to 100 mg/m<sup>3</sup> but then decreased with a further increase of input concentrations from 100 to 120 mg/m<sup>3</sup>.

Langmuir and Freundlich adsorption isotherm models were established to determine the parameters of H<sub>2</sub>S adsorption by RM8S-1.5. As summarized in Table 1, the adsorption of H<sub>2</sub>S on RM8S-1.5 is more fitted with Langmuir (R<sup>2</sup> = 0.906) than with the Freundlich isotherm adsorption model (R<sup>2</sup> = 0.781). This implied that the adsorption of H<sub>2</sub>S on RM8S-1.5 not only physical adsorption by electrostatic attraction but also chemical interaction of H<sub>2</sub>S and oxides of iron and aluminum formed after calcined at a high temperature of 800 °C. The maximum adsorption capacity was calculated to be 36.68 mg/g.

To evaluate if an adsorption process is fitted with the single-layer adsorption model described by Langmuir equation, it is required to be evaluated through equilibrium parameter R<sub>L</sub><sup>17</sup>, as expressed in Equation (1). Results from Table 2 with R<sub>L</sub> < 1 confirmed the suitability of the Langmuir isotherm model for H<sub>2</sub>S adsorption by RM8S-1.5 in this input concentration range.

$$R_L = \frac{1}{1 + K_L C_0} \quad (1)$$



**Figure 1:** Schematic for H<sub>2</sub>S adsorption test Diagram of research model: (1) preliminary treatment, (2) H<sub>2</sub>SO<sub>4</sub> tank, (3) Na<sub>2</sub>S tank, (4) adsorption column, (5) air pump, (6) tee, (7) flowmeter, (8) impinger

**Table 1: Parameters of frendlich and langmuir isotherms**

Freundlich isotherm		
n	$K_f \text{ (mg/g) / (mg/m}^3)^{1/n}$	$R^2$
0.392	4.427	0.782
Langmuir isotherm		
$a_{max} \text{ (mg/g)}$	$K_L \text{ (m}^3/\text{mg)}$	$R^2$
36.68	0.0270	0.906

**Table 2: Value of  $R_L$  with different concentrations**

$C_o$	45.13	63.78	85.74	105.71	126.16
$R_L$	0.45	0.37	0.30	0.26	0.23

Where  $K_L$  is the mass transfer coefficient according to the Langmuir equation and  $C_o$  is input concentration.

### Influence of input flow rate

This experiment was carried out with the flow rate in a range of 1.0 - 3.0 L/min and an input concentration of 100 - 110 mg/m<sup>3</sup>. Obviously, the adsorption capacity continuously decreased from 30.49 mg/g to 16.58 mg/g with an increase of flow rate from 1.0 to 3.0 L/min (Figure 4). This is because of the decrease of contact time between H<sub>2</sub>S and adsorbent with the increase of gas flow rate, which leads to the low H<sub>2</sub>S adsorption on the surface of RM8S-1.5 material.

### Regeneration of adsorbent

The recycle test was also conducted to investigate the effect of the desorption process on the sorption capacity of RM8S-1.5 material. The desorption process was carried out by drying saturated RM8S-1.5 samples at

200 and 400 °C for 20 min. After desorption, the material was cooled and then reused for adsorption. As presented in Figure 5, the capacity of the regenerated materials was lower than the original one although still at high levels. The adsorption capacity of material regenerated at 400 °C was higher than that at 200 °C. However, the difference was not much since capacity increased only from 24.0 to 26.9 mg/g as compared to double temperature with higher energy consumption.

## CONCLUSION

Adsorbents from red mud were successfully synthesized and applied for H<sub>2</sub>S adsorption. Results showed that adsorption capacity increased with the increase of calcination temperature and H<sub>2</sub>SO<sub>4</sub> was better than HCl for red mud activation. The highest adsorption capacity of 30.49 mg/g was achieved at input concentration of 100 mg/m<sup>3</sup> and flow rate of 1 L/min using red mud calcined at 800 °C and activated with 1.5

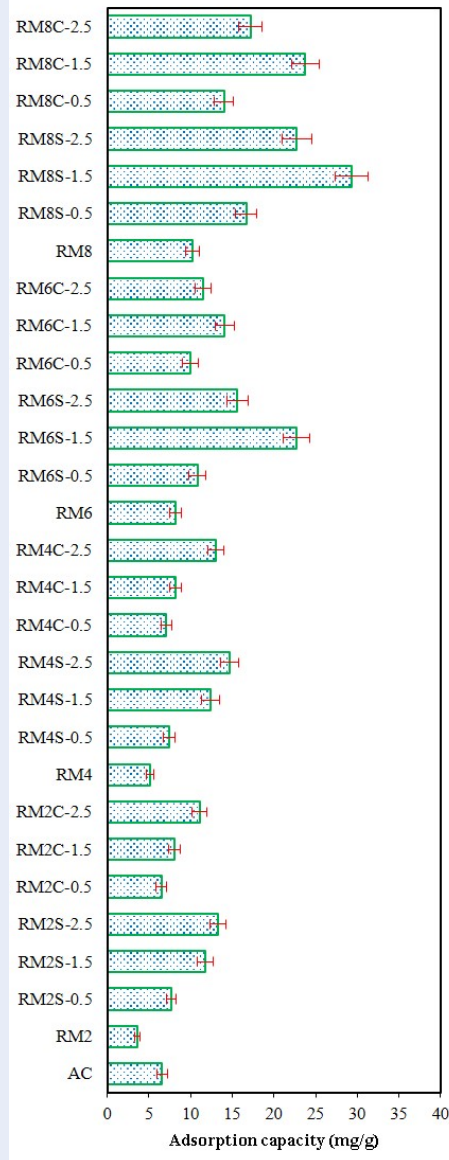


Figure 2: H<sub>2</sub>S adsorption capacity of different materials

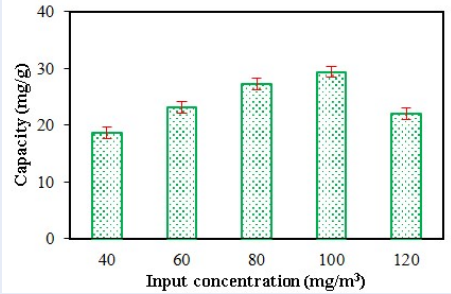


Figure 3: Adsorption capacity of RM8S-1.5 at different input concentrations

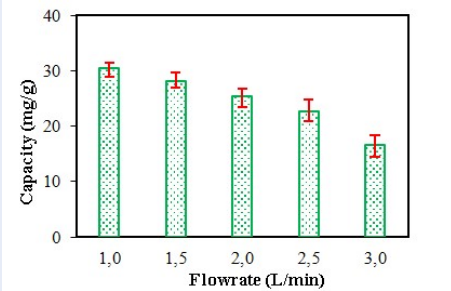


Figure 4: Adsorption capacity of RM8S-1.5 with different gas flow rates

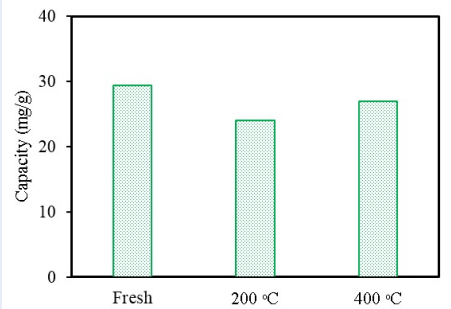


Figure 5: H<sub>2</sub>S adsorption result of RM8S-1.5 material after desorption at different temperatures

M H<sub>2</sub>SO<sub>4</sub> solution. The adsorption process follows Langmuir ( $R^2 = 0.906$ ) rather than the Freundlich adsorption model. Moreover, the material can be regenerated by thermal treatment at 200 °C with 81.7% capacity. These results suggest a potential use of activated red mud for H<sub>2</sub>S and maybe other gases treatment.

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### ABBREVIATION

AC: activated carbon

RM: red mud

RMX: red mud activated at X00 °C

RMXC-Y: red mud activated at X00 °C and by HCl with concentration of Y (M)

RMXS-Y: red mud activated at X00 °C and by H<sub>2</sub>SO<sub>4</sub> with concentration of Y (M)

## CONFLICT OF INTEREST

There is no conflict of interest regarding this manuscript.

## AUTHOR CONTRIBUTION

Lam Pham Thanh Hien helped with funding, planned the experiment, and prepared the draft manuscript.

Le Truong Anh Huy, Pham Dan Thanh, Le Nguyen Dang Khoa, Bui Khanh Le, Le Thi Kieu Thi, Vo Thi Thanh Thuy did the experiment, collected, and composed data.

Nguyen Nhat Huy outlined the research, prepared the figures, and completed the manuscript.

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# Nghiên cứu chế tạo vật liệu bùn đỏ hoạt hóa ứng dụng hấp phụ H<sub>2</sub>S trong khí thải

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#### TÓM TẮT

Bùn đỏ là một loại chất thải rắn có tính kiềm cao phát sinh từ quá trình sản xuất nhôm từ quy trình Bayer. Các hồ chứa bùn đỏ thường được xem là rủi ro môi trường tiềm tàng. Việc xử lý bùn đỏ khá tốn kém do chưa có một công nghệ hiệu quả và kinh tế. Mặt khác, thành phần chính của bùn đỏ bao gồm Fe<sub>2</sub>O<sub>3</sub>, Al<sub>2</sub>O<sub>3</sub>, SiO<sub>2</sub>, và Na<sub>2</sub>O có thể sử dụng như những tiền chất để chế tạo các loại vật liệu nano. Nghiên cứu này được thực hiện nhằm đánh giá khả năng hoạt hóa bùn đỏ và ứng dụng để xử lý chất ô nhiễm H<sub>2</sub>S trong khí thải. Bùn đỏ được hoạt hóa ở các nhiệt độ khác nhau, với các loại axit khác nhau và ở các nồng độ khác nhau. Bùn đỏ hoạt hóa sau đó được sử dụng để hấp phụ khí thải H<sub>2</sub>S trong không khí với nồng độ từ 90 đến 110 mg/m<sup>3</sup> sử dụng cột hấp phụ tầng tĩnh. Kết quả cho thấy bùn đỏ hoạt hóa ở 800 °C sử dụng axit H<sub>2</sub>SO<sub>4</sub> ở nồng độ 1,5 M cho hiệu quả xử lý H<sub>2</sub>S cao nhất. Hiệu suất hấp phụ trung bình ở mức 80,2 % và dung lượng hấp phụ đạt đến 29,38 mgH<sub>2</sub>S/g bùn đỏ hoạt hóa. Ảnh hưởng của lưu lượng dòng khí và nồng độ đầu vào lên quá trình hấp phụ cũng được khảo sát và kết quả chỉ ra rằng hiệu suất hấp phụ cao nhất ở nồng độ H<sub>2</sub>S đầu vào 100 mg/m<sup>3</sup> và lưu lượng 1 L/phút. Mô hình hấp phụ đẳng nhiệt Langmuir và Freundlich đã được áp dụng để mô tả quá trình hấp phụ và kết quả thực nghiệm cho thấy quá trình hấp phụ H<sub>2</sub>S sử dụng bùn đỏ hoạt hóa phù hợp hơn với mô hình Langmuir. Thí nghiệm giải hấp và độ bền vật liệu cũng đã được thực hiện để đánh giá khả năng ứng dụng thực tế của vật liệu bùn đỏ hoạt hóa và nhiệt độ giải hấp được đề xuất ở 200 °C tương ứng với khả năng hấp phụ đạt 81.7% dung lượng hấp phụ ban đầu.

**Từ khóa:** Bùn đỏ, hydro sulfua, hấp phụ, xử lý khí thải

**Trích dẫn bài báo này:** Hiền L P T, Huy L T A, Thanh P D, Khoa L N D, Lê B K, Thi L T K, Thùy V T T, Huy N N. Nghiên cứu chế tạo vật liệu bùn đỏ hoạt hóa ứng dụng hấp phụ H<sub>2</sub>S trong khí thải. *Sci. Tech. Dev. J. - Eng. Tech.*; 2(S12):S140-S145.