Investigate the effects of the dimensional factors on resistance force in magnetorheological brake with the waveform boundary of a rotary disk

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ABSTRACT

There are many studies on applying magneto-rheological fluid (MRF) to braking systems and shock absorbers. This paper investigates the resistance caused by the MRF to the curved surface of the brake components to improve the braking and damping forces. MRF is also called a smart fluid whose viscosity can be controlled. This study uses the proposed model of the magnetorheological brake (MRB) of Nam and Ahn with the waveform boundary of a rotary disk. In this study, the Taguchi method is applied to build virtual experiments and investigate the influence of dimensional parameters of the brake component, including the radius of arc (Rrac), MRF gap (g), and the thickness of the part (b) on its resistance force (F). The resistance force caused by a non-planar surface's resistance is expected to be significantly larger than that of a flat surface. Overall, the results show that the MRF gap g (mm) has the most significant influence, followed by the radius of the arc (Rarc) and, then, the thickness (b) of the components. Thus, based on these parameters' effects, there will be a practical direction to improve the design of devices using this kind of MRF special brake or clutch. **Key words:** magneto-rheological fluid (MRF), magnetorheological brake (MRB), fluid gap, waveshaped boundary, resistance force

INTRODUCTION

There many studies related to improving braking momentum in MRF-based brakes in recent years ^{1–22}. In particular, several studies have directly examined the behavior of magnetic fields to cover a large area to increase the brake force.

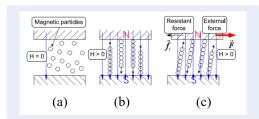


Figure 1: MRF behaviors in a change of magnetic field ². (a)Without a magnetic field. (b)With a magnetic field and without sliding. (c) With magnetic field and sliding

Magnetorheological fluid (MRF) is an attractive, smart material widely used to develop devices in various industries, including automotive engineering, aerospace engineering, manufacturing, and medical fields. A typical MRF is a type of functional fluid that has a suspension of magnetic particles in inert carrier

liquids. The particles, typically with a size in the order of 1-10 µm, are added to the fluid, such as mineral or silicone oils. MRF also contains small amounts of additives that affect the polarization of the particles or stabilization of the structure of the suspension to resist settling. The behavior of MRF is shown in Figure 1. When a field normally orients to the direction of the flow, the magnetic particles are arranged to form many parallel chains (fibrils) and placed across the flow. These fibrils are broken in some instances by the fluid flow, and the broken fibrils are reconnected to the next adjacent fibrils by the applied magnetic field, which is proportional to the shear stress τ . The fibrils cause the production of shear stress, which is largely independent of the strain rate. This is commonly referred to as the yield stress and is denoted as $\tau_{\rm v}^2$. Through this shear stress, the resistant force is generated and controlled by the magnetic field. The is largely independent of the strain rate. This is commonly referred to as the yield stress and is denoted as τy^2 . Through this shear stress, the resistant force is generated and controlled by the magnetic field. The Bingham plastic model has the stress-strain rate relation of τ shown in equation (1) with the magnetic field B, dynamic viscosity η , and strain rate $\dot{\gamma} = \partial u/\partial y$.

$$\tau = \tau_Y(B) + \eta \dot{\gamma} \tag{1}$$

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Some typical devices using MRF are Magnetorheological Brake (MRB), Magnetorheological Clutch (MRC), and Magnetorheological Damper (MRD). Furthermore, an MRF-based device possesses a distinctive advantage not found in conventional devices like servomotors and hydraulic machines, namely, the fail-safe function. This means that even in the event of failure during control action, MRF devices can continue to deliver passive device performance. This unique feature is made possible due to the presence of a carrier liquid in the MRF device, which serves a similar role as the viscous oil commonly employed in passive devices.

MRF-based brakes identified many different structural configurations to improve the effect of these smart fluids. Hung et al. 15 made a notable enhancement by altering the coil layout design to augment both the coverage area and magnetic field strength in the active region of the fluid. In addition, some models increase the number of brake discs to increase the contact area of the liquid and the surface 15. Nam et al. 2 proposed an MRB incorporating a brake disk with a wave-shaped boundary (Figure 2), which provides braking torque produced by the effects of the material deformation process. The results illustrate that the output torque with this kind of structure is close to 600% larger than that of conventional brakes of the same size. Similar to Nam, C. Sarkar et al. 7 used a parabolic-shaped rotating disc. In another study, A. Singh et al. 17 focused on a wedge-shaped MRC.

This paper proposes a simple equivalent model to investigate in detail the interaction between the conventional structure and the curve form. The simulation only estimates the values of the magnetic field to calculate the output resistance force. It is used to evaluate the influencing factors that affect the output force. In this case, since this is a simulation case only, the liquid covered will be neglected. An ANOVA statistic was performed to quantify the influence of the three input parameters, which are the MRF gap (g), radius (Rarc) of the arc, and thickness (b) of the components.

MATERIALS AND METHODS

In this paper, the Taguchi method is used to set up the virtual experiment; The virtual model shown in Figure 3 is a simple element of the waveform boundary of a rotary disk, which is proposed in Nam *et al.* (2009) ¹. This model includes the gap-filled MRF (also called MRF gap) between sliding and fixed parts. The magnetic field will be applied to the MRF gap and varied by the coil through the magnetic core. In the proposed virtual experiment, three operating factors include the radius of the arc (Rarc), the fluid gap (g) between, and the thickness (b) of the observing object.

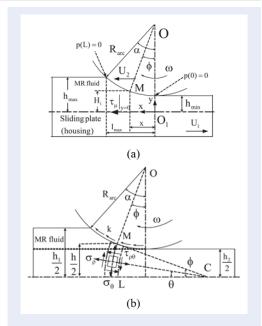
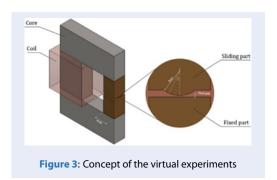


Figure 2: Nam *et al.* model [2]. a) The resistance force caused by the sliding process. b) The resistance force caused by the deforming process.

The factors and their levels have been chosen according to a literature review of previous publications on the radius of the curve and the MRF¹. For the design of experiments with three factors and three levels for each factor, a standard L27 orthogonal array was applied. To avoid systematic bias, the sequence in which these runs were carried out was randomized. The statistical analysis of the results was carried out using DoE in Minitab.

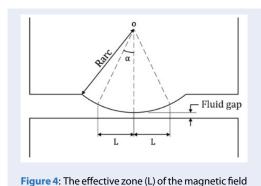


In this research, the Taguchi method is applied to examine which parameters affect the resultant resistance force caused by magneto-rheological fluid on the curve of the sliding part. The benefit of this method is that a minimal number of experiments are needed to study the effect factors on a pair of parameters. The levels of selected factors are shown in Table 1.

Table 1: Selected Factors and Levels

Factor	Unit		Level		
		1	2	3	
Radius of arc (Rarc)	mm	4	5.5	7	
MRF gap (g)	mm	0.2	0.5	0.8	
Width of part (b)	mm	10	15	20	

Steel 1008 is used for the core in this simulation model, and the MRF-132DG of Lord Corp. is applied for the MRF. The purpose of these samples is to facilitate the easy setting and measurement of output force. However, it is not changing the meaning of this study. When the applied magnetic field is caused by the coil, which has an NI of around 200-ampere turns, the behavior and value of the magnetic field (H) response in each sample are different. The magnetic field (H) value is averaged in the range L of the effective angle $\alpha \leq 15^o$ in the deforming process and sliding 1 . Figure 4 shows the effective zone (L) of the magnetic field defined by the angle of α in the MRF gap.



is defined by the angle of in the MRF gap.

When applying a magnetic field, the general force per unit width of the arc is the sum of resistance forces in both models shown in equation (2). Where F is a resistance force; $F_{drawing}$ is force caused by deformation theory $F_{\tau\ (B)}$ is force generated from the sliding process; and B is the thickness of the sliding part. In addition, the effect of mechanical friction, such as seal friction, bearing friction, and so forth, is neglected.

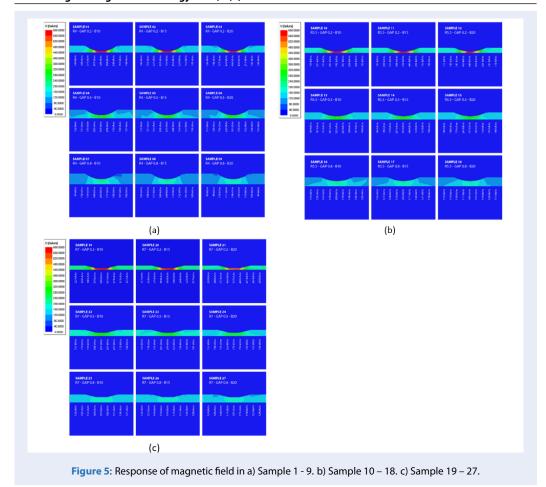
$$F = (F_{drawing} + F_{\tau(B)}).B \tag{2}$$

RESULTS

The simulation results with the resistance force value (N) of the corresponding numbered test after calculation are described in Table 2 and Figure 5. In Table 2, the test samples No. 21, 20, 12, and 24 have obtained generated force by MRF which is higher than the others and have input parameters in bold rows.

Table 2: Simulation results

Sample No.	Radius of arc, Rarc (mm)	MRF gap, g (mm)	Thickness, b (mm)	Resistance Force, F
1	4.00	0.20	10.00	7.58
2	4.00	0.20	15.00	11.38
3	4.00	0.20	20.00	15.17
4	4.00	0.50	10.00	4.71
5	4.00	0.50	15.00	7.03
6	4.00	0.50	20.00	9.31
7	4.00	0.80	10.00	3.31
8	4.00	0.80	15.00	4.90
9	4.00	0.80	20.00	6.51
10	5.50	0.20	10.00	11.94
11	5.50	0.20	15.00	17.91
12	5.50	0.20	20.00	23.88
13	5.50	0.50	10.00	7.67
14	5.50	0.50	15.00	11.47
15	5.50	0.50	20.00	15.23
16	5.50	0.80	10.00	5.36
17	5.50	0.80	15.00	7.97
18	5.50	0.80	20.00	10.46
19	7.00	0.20	10.00	16.62
20	7.00	0.20	15.00	24.94
21	7.00	0.20	20.00	33.25
22	7.00	0.50	10.00	11.04
23	7.00	0.50	15.00	16.48
24	7.00	0.50	20.00	21.86
25	7.00	0.80	10.00	7.80
26	7.00	0.80	15.00	11.57
27	7.00	0.80	20.00	15.27



DISCUSSION

To understand the influence of each factor with different levels on the resistance force (N), the average S/N ratios in each group were calculated and listed in Table 3. The average S/N ratios in Table 3 are plotted in Figure 6. The range of each factor (delta) is defined as the difference between the highest and the lowest average S/N ratios; the more extensive the range, the more significant influence of the corresponding factor on the surface quality.

For more details, the results of the ANOVA with resistance force are presented in Table 4. The results of this analysis are performed at a significance level of α = 0.05, i.e., with a confidence level of 95%. Test samples No. 21, 20, 12, and 24 show that the study's potential is apparent with the values of 33.25, 24.94, 23.88, and 21.86 N of force, respectively. Using the simple load-cell test bench can help in experimental testing, which is not the focus here.

In this study, MRF gap g is the most influential factor (34.78%), and the change in output force occurs very

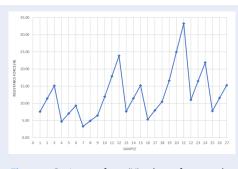


Figure 6: Resistance force (N) values of 27 samples

strongly in the range from 0.2 to 0.8 mm. The radius of the arc is the second most influential factor, with a 33.40% influence on output force. Thickness has the smallest range and has the most minor impact, 1.38%, on the generated resistance force.

By following the criteria of a more significant resistance force with a larger S/N ratio, Figure 7 with marked red circles can be used to determine the opti-

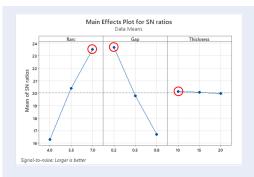


Figure 7: Influence of dimensional parameter according to the survey values on the resistance forceindex F.

mal factors to achieve the maximum force. The combination to achieve the most significant output force is a radius of 7.0 mm (level 3), a fluid gap of 0.2 mm (level 1), and a thickness of 10 mm (level 1). This will be a significant key for designing the new MRB using the waveform boundary of the rotary disk.

Table 3: Response Table for Signal-to-Noise Ratios

	•		
Level	Radius of arc, Rarc	MRF gap, g	Thickness,
1	16.27	23.67	20.13
2	20.4	19.8	20.07
3	23.49	16.7	19.96
Delta	7.22	6.96	0.17
Rank	1	2	3

Table 4: Analysis of variance (ANOVA) for Resistance Force

Source	DF	Adj SS	Adj SS (%)	Adj MS	F- Value	P- Value
Radius of arc	2	439.64	33.40	219.822	10.98	0.001
MRF gap	2	458.00	34.78	228.999	11.44	0.000
Thickness	2	18.19	1.38	9.093	0.45	0.641
Error	20			20.014		
Total	26	1316.1	0			

The thickness parameter shows that it shows a distrust P-value larger than 0.05. The number of samples may be a big reason for this. In addition, expanding the

range of the variable Rarc and Fluid gap is necessary for further conclusions. However, increasing the radius of the arc until the curve becomes linear will neglect the effect of deforming processes. On the other hand, the fluid gap is the most challenging part of manufacturing because the tolerance limitation must be well controlled for the number of 0.2 mm. Therefore, the range of these parameters should be discovered in further research for optimizing the output resistance force in MRF-based brake systems.

CONCLUSIONS

The findings of this study hold the potential to make substantial contributions to the development and production of sliding components in MRB. The resistance force can be varied by fine-tuning the input current, thickness, and fluid properties, resulting in enhanced overall performance. With optimization efforts in parameters with maximum resistance force, the design has the potential to bring about increased energy efficiency across diverse industrial and engineering implementations.

By simulation using Minitab and Ansys Maxwell, the paper shows that MRF gap g is the most influential factor, the radius of the arc Rarc is the second most influential factor, and the thickness b has less impact on the generated resistance force in the structure of a brake disk with a wave-shaped boundary.

Based on these results, the optimal design of MRB using the wave-shaped boundary of a rotary disk will be focused on in the next studies. It will compare the outcomes of the simulation model with those of the physical model.

ABBREVIATIONS

MRF: Magneto-Rheological Fluid MRB: Magneto-Rheological Brake MRC: Magneto-Rheological Clutch MRD: Magneto-Rheological Damper

COMPETING INTERESTS

The authors wish to confirm that there are no known conflicts of interest associated with this publication, and there has been no significant financial support for this work that could have influenced its outcome.

AUTHORS' CONTRIBUTIONS

The first author (T. H. Nam) conceived of the study, the second author (D. N. H. Long) participated in its design and simulation, and helped to draft the manuscript. The authors read and approved the final manuscript.

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REFERENCES

- Nam TH, Ahn KK. New Approach to Designing an MR Brake Using a Small Steel Roller and MR Fluid. Journal of Mechanical Science and Technology. 2009;23:1911–1923.
- Nam TH, Ahn KK. A new structure of a magnetorheological brake with the waveform boundary of a rotary disk. Smart Mater Struct. 2009;18:115029.
- Sarkar C, Hirani H. Theoretical and Experimental Studies on a Magnetorheological Brake Operating Under Compression Plus Shear Mode. Smart Materials and Structures. 2013;22:115032.
- Sarkar C, Hirani H. Design of a Squeeze Film Magnetorheological Brake Considering Compression Enhanced Shear Yield Stress of Magnetorheological Fluid. J Phys: Conf Ser. 2013;412:012045. Available from: https://doi.org/10.1088/ 1742-6596/412/1/012045
- Shiao Y, Anh QN. Torque Enhancement for a New Magnetorheological Brake. Procedia Engineering. 2014;76:12–23.
- Shiao Y, Nguyen QA. Structural Analysis and Validation of the Multi-pole Magnetorheological Brake for Motorcycles. Procedia Engineering. 2014;76:24–34.
- Sarkar C, Hirani H. Design of Magnetorheological Brake using Parabolic Shaped Rotating Disc. Proceedings of the Institution of Mechanical Engineers, Part L: Journal of Materials: Design and Applications. 2020;243(9):1252–1266. Available from: https://doi.org/10.1177/1464420720931886.
- Attia EM, Elsodany NM, El-Gamal HA, Elgohary MA. Theoretical and Experimental Study of Magneto-Rheological Fluid Disc Brake. Alexandria Engineering Journal. 2017;56:189–200.
- Hu G, Lu Y, Sun S, Li W. Development of a Self-Sensing Magnetorheological Damper with Magnets In-Line Coil Mechanism. Sensors and Actuators A. 2017;255:71–78.
- Lydia RS, Mokhtar R, Husaini ABM, Norhaniza BJ. Design and Development of Coil Casing MRF Brake System. MATEC Web of Conferences. 2017;90:01017.

- Hamdan LH, Mazlan SA, Imaduddin F, Sarip S, Yusop A. Simulation Studies of a New Magnetorheological Brake with Difference Gap Size Using Combination of Shear and Squeeze Mode. Engineering Applications for New Materials and Technologies. 2018;p. 413–424. Available from: https://doi.org/10.1088/1742-6596/412/1/012045.
- George LK, Tamilarasan N, Thirumalini S. Design and Analysis of Magneto Rheological Fluid Brake for an all Terrain Vehicle. IOP Conf Series Materials Science and Engineering. 2018;310:012127.
- Thang H, Dung H. Optimization Design Magnetorheological Brake with Multiple Disk. Tap Chí Khoa Học và Công Nghệ Đại Học Đà Nẵng, ISSN 1859-1531. 2019;17(1.2).
- Wang H, Bi C. Study of a Magnetorheological Brake Under Compression-Shear Mode. Smart Mater Struct, IOP. 2020:29:1–17.
- Quoc NV, Tuan LD, Hiep LD, Q HN, Choi SB. Material Characterization of MR Fluid on Performance of MRF Based Brake. Frontiers in Materials. 2019;6.
- Jinaga R, Thimmaiah J, Shreedhar K, B CS. Design, Fabrication and Testing of a Magneto-rheological Fluid Braking System for Machine Tool Application. SN Applied Sciences. 2019;1328.
- Singh A, Thakur MK, Sarkar C. Design and Development of a Wedge Shaped Magneto-Rheological Clutch. Proceedings of the Institution of Mechanical Engineers, Part L: Journal of Materials: Design and Applications. 2020;234(9):1252–1266.
- Hu G, Wu L, Li L, Yu L. Performance Analysis of Rotary Magnetorheological Brake with Multiple Fluid Flow Channels. IEEE Access. 2020:8.
- Acharya S, Saini TRS, S V, Kumar H. Selection of Optimal Composition of MR Fluid for a Brake Designed using MOGA Optimization Coupled with Magnetic FEA Analysis. Journal of Intelligent Material Systems. 2021;32(16):1831–1854. Available from: https://doi.org/10.1177/1045389X20977905.
- Tri DB. Phát triển hệ thống phản hồi lực dùng lưu chất từ biến, Tóm tắt Luận án Tiến sĩ, Trường ĐH Sư phạm Kỹ thuật Tp.HCM. 2021:.
- Hu G, Wu L, Li L. Torque Characteristics Analysis of a Magnetorheological Brake with Double Brake Disc. Actuators. 2021;10:23,.
- Chen S, Chen W, Huang J. Study of Variable Thickness Magnetorheological Transmission Performance of Electrothermal Shape Memory Alloy Squeeze. Appl Sci. 2022;12:4297.

Nghiên cứu ảnh hưởng của các yếu tố kích thước đối với lực cản trong phanh từ lưu biến với đĩa quay có biên dạng sóng

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TÓM TẮT

Có nhiều nghiên cứu ứng dụng chất lưu từ biến (MRF) vào hệ thống phanh và giảm xóc. Bài báo này nghiên cứu lực cản do MRF gây ra đối với bề mặt đường cong của các bộ phận phanh để cải thiện lực phanh và giảm chấn. MRF còn được gọi là chất lỏng thông minh có thể kiểm soát độ nhớt. Nghiên cứu này sử dụng mô hình phanh từ lưu biến (MRB) được đề xuất bởi Nam và Ahn với biên dạng sóng của một đĩa quay. Trong nghiên cứu này, phương pháp Taguchi được áp dụng để xây dựng thí nghiệm ảo và khảo sát sự ảnh hưởng của các thông số kích thước của chi tiết phanh bao gồm bán kính cung Rrac (mm), khe hở MRF g (mm), chiều dày của chi tiết b (mm) đến lực cản được tạo ra của nó (N). Lực cản tổng hợp gây ra bởi trở lực của một bề mặt không phẳng dự kiến sẽ lớn hơn đáng kể so với lực cản của một bề mặt phẳng. Nhìn chung, kết quả cho thấy khe hở MRF g (mm) có ảnh hưởng đáng kể nhất, tiếp theo là bán kính cung Rarc (mm) và sau đó là độ dày b (mm) của các chi tiết. Như vậy, trên cơ sở ảnh hưởng của các thông số này sẽ có hướng thiết thực để cải tiến thiết kế các thiết bị phanh hoặc ly hợp đặc chủng sử dụng MRF dạng này.

Từ khoá: chất lưu từ biến (MRF), phanh từ lưu biến (MRB), khe chứa lưu chất, biên dạng sóng, lực cản trở

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